## feATURES

- Broadband RF, LO and IF Operation
- High Input IP3: >20dBm from 30MHz to 900MHz +17 dBm at 1900 MHz
- Typical Conversion Gain: 1dB
- SSB Noise Figure: 11dB at 900 MHz

14 dB at 1900 MHz

- Integrated LO Buffer: Insensitive to LO Drive Level
- Single-Ended or Differential LO Drive
- High LO-RF Isolation
- Enable Function
- 4.5V to 5.25V Supply Voltage Range
- $4 \mathrm{~mm} \times 4 \mathrm{~mm}$ QFN Package


## APPLICATIONS

- HF/VHF/UHF Mixer
- Cellular/PCS/UMTS Infrastructure
- High Linearity Mixer Applications
- ISM Band Receivers
- Wireless Medical Telemetry System (WMTS)


## DESCRIPTIOn

The $\mathrm{LT}{ }^{\circledR} 5512$ is an active double-balanced mixer IC, optimized for high linearity HF, VHF and UHF applications. The IC includes an integrated LO buffer amplifier to drive the mixer and an RF buffer amplifier for improved LO-RF isolation. Internal bias circuits eliminate the need for precision external resistors and allow the device to be powered-down using the enable control (EN) pin.

The externally matched RF and IF ports allow the mixer to be used at very low frequencies, below 1 MHz or up to 3GHz. The differential LO input is designed for single-ended or a differential input drive.

The LT5512 is a high-linearity alternative to passive diode mixers. Unlike passive mixers, which have conversion loss and require high LO drive levels, the LT5512 delivers conversion gain and requires significantly lower LO drive levels.
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## TYPICAL APPLICATION

High Signal-Level Downmixer for 600MHz Wireless Medical Telemetry System
Conv Gain, IIP3, NF and LO Leakage vs LO Power

ABSOLUTG MAXIMUM RATInGS(Note 1)
Supply Voltage ( $\mathrm{V}_{\mathrm{CC} 1}, \mathrm{~V}_{\mathrm{CC} 2}, \mathrm{IF}^{+}, \mathrm{IF}^{-}$). ..... 5.5V
Enable Voltage

$\qquad$
-0.3 V to $\mathrm{V}_{\mathrm{CC}}+0.3 \mathrm{~V}$
$\mathrm{LO}^{+}$to $\mathrm{LO}^{-}$Differential Voltage ..... $\pm 1.5 \mathrm{~V}$
(+6dBm equivalent)
RF $^{+}$to RF-$^{-}$Differential Voltage ..... $\pm 0.7 \mathrm{~V}$
(+11dBm equivalent)
Operating Temperature Range ..... $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$
Storage Temperature Range $-65^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$Junction Temperature ( $\mathrm{T}_{\mathrm{J}}$ )$125^{\circ} \mathrm{C}$

PACKAGE/ORDER INFORMATION

|  |  |
| :---: | :---: |
| ORDER PART NUMBER | PART MARKING |
| LT5512EUF | 5512 |
| Order Options Tape and Reel: Add \#TR Lead Free: Add \#PBF Lead Free Tape and Reel: Add \#TRPBF Lead Free Part Marking: http://www.linear.com/leadfree/ |  |

Consult LTC Marketing for parts specified with wider operating temperature ranges.

## DC ELECTRICAL CHARACTERISTICS <br> (Test Circuit Shown in Figure 2) $\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}$, $\mathrm{EN}=$ High,

$\mathrm{T}_{A}=25^{\circ} \mathrm{C}$ (Note 3), unless otherwise noted.

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Enable (EN) Low = Off, High = On |  |  |  |  |  |
| Turn On Time |  |  | 3 |  | $\mu \mathrm{S}$ |
| Turn Off Time |  |  | 13 |  | $\mu \mathrm{S}$ |
| Input Current | $V_{\text {ENABLE }}=5 \mathrm{~V}$ |  | 50 |  | $\mu \mathrm{A}$ |
| Enable = High (On) |  | 3 |  |  | V |
| Enable = Low (Off) |  |  |  | 0.3 | V |
| Power Supply Requirements ( $\mathrm{V}_{\text {cc }}$ ) |  |  |  |  |  |
| Supply Voltage |  | 4.5 |  | 5.25 | V |
| Supply Current |  |  | 56 | 74 | mA |
| Shutdown Current | EN = Low |  |  | 100 | $\mu \mathrm{A}$ |

## AC ELECTRICAL CHARACTERISTICS

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :--- | :--- | :---: | :---: | :---: | :---: |
| RF Input Frequency Range | Requires Appropriate Matching | 0.001 to 3000 | MHz |  |  |
| LO Input Frequency Range | Requires Appropriate Matching | 0.001 to 3000 | MHz |  |  |
| IF Output Frequency Range | Requires Appropriate Matching | 0.001 to 2000 | MHz |  |  |
| LO Input Power | 1 kHz to 1700 MHz (Resistive Match) | -11 | -5 | 1 | dBm |
|  | 1200 MHz to 3000 MHz (Reactive Match) | -18 | -10 | -2 | dBm |

AC ELECTRICAL CHARACTERISTICS
Downmixer Applications: (Test Circuits Shown in Figures 1 and 2)
$V_{C C}=5 V, E N=H i g h, T_{A}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{RF}}=-10 \mathrm{dBm}(-10 \mathrm{dBm} /$ tone for two-tone IIP3 tests, $\Delta f=200 \mathrm{kHz}$ ), High-Side LO at -5 dBm for 45MHz, 140 MHz and 450 MHz tests, Low-Side LO at -10 dBm for $900 \mathrm{MHz}, 1900 \mathrm{MHz}$ and 2450 MHz tests, unless otherwise noted.
(Note 2, 3 and 4)

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Conversion Gain | $\begin{aligned} & \hline R F=45 \mathrm{MHz}, I F=2 \mathrm{MHz} \\ & R F=140 \mathrm{MHz}, \mathrm{IF}=10 \mathrm{MHz} \\ & R F=450 \mathrm{MHz}, \mathrm{IF}=70 \mathrm{MHz} \\ & R F=900 \mathrm{MHz}, \mathrm{IF}=170 \mathrm{MHz} \\ & R F=1900 \mathrm{MHz}, \mathrm{IF}=170 \mathrm{MHz} \\ & R \mathrm{RF}=2450 \mathrm{MHz}, \mathrm{IF}=240 \mathrm{MHz} \end{aligned}$ | -1 | $\begin{gathered} 1 \\ 2 \\ 1.1 \\ 0 \\ 1 \\ 2 \end{gathered}$ |  | dB $d B$ $d B$ $d B$ $d B$ $d B$ |
| Conversion Gain vs Temperature | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}, \mathrm{RF}=900 \mathrm{MHz}$ |  | -0.011 |  | $\mathrm{dB} /{ }^{\circ} \mathrm{C}$ |
| Input 3rd Order Intercept | $\begin{aligned} & \mathrm{RF}=45 \mathrm{MHz}, \mathrm{IF}=2 \mathrm{MHz} \\ & R F=140 \mathrm{MHz}, \mathrm{IF}=10 \mathrm{MHz} \\ & R F=450 \mathrm{MHz}, I \mathrm{IF}=70 \mathrm{MHz} \\ & R F=900 \mathrm{MHz}, \mathrm{IF}=170 \mathrm{MHz} \\ & R F=1900 \mathrm{MHz}, \mathrm{IF}=170 \mathrm{MHz} \\ & R F=2450 \mathrm{MHz}, I \mathrm{IF}=240 \mathrm{MHz} \end{aligned}$ |  | $\begin{gathered} 20.4 \\ 20.7 \\ 21.3 \\ 21 \\ 17 \\ 13 \end{gathered}$ |  | dBm <br> dBm <br> dBm <br> dBm <br> dBm <br> dBm |
| Single-Sideband Noise Figure | $\begin{aligned} & \mathrm{RF}=140 \mathrm{MHz}, \mathrm{IF}=10 \mathrm{MHz} \\ & R F=450 \mathrm{MHz}, \mathrm{IF}=70 \mathrm{MHz} \\ & R F=900 \mathrm{MHz}, \mathrm{IF}=170 \mathrm{MHz} \\ & R F=1900 \mathrm{MHz}, \mathrm{IF}=170 \mathrm{MHz} \\ & R F=2450 \mathrm{MHz}, \mathrm{IF}=240 \mathrm{MHz} \end{aligned}$ |  | $\begin{gathered} 10.3 \\ 10.3 \\ 11 \\ 14 \\ 13.4 \end{gathered}$ |  | dB dB dB dB $d B$ |
| LO to RF Leakage | $\mathrm{f}_{\mathrm{LO}}=250 \mathrm{kHz}$ to 700 MHz (Figure 1) $\mathrm{f}_{\mathrm{L} 0}=700 \mathrm{MHz}$ to 2500 MHz (Figure 2) |  | $\begin{aligned} & \leq-63 \\ & \leq-50 \end{aligned}$ |  | $\begin{aligned} & \mathrm{dBm} \\ & \mathrm{dBm} \\ & \hline \end{aligned}$ |
| LO to IF Leakage | $\mathrm{f}_{\mathrm{LO}}=250 \mathrm{kHz}$ to 500 MHz (Figure 1) <br> $\mathrm{f}_{\mathrm{LO}}=500 \mathrm{MHz}$ to 1250 MHz (Figure 1) <br> $\mathrm{f}_{\mathrm{LO}}=700 \mathrm{MHz}$ to 1500 MHz (Figure 2) <br> $\mathrm{f}_{\mathrm{L} 0}=1500 \mathrm{MHz}$ to 1950 MHz (Figure 2) <br> $\mathrm{f}_{\mathrm{L} 0}=1950 \mathrm{MHz}$ to 2500 MHz (Figure 2) |  | $\begin{aligned} & \leq-35 \\ & \leq-40 \\ & \leq-45 \\ & \leq-40 \\ & \leq-32 \end{aligned}$ |  | dBm <br> dBm <br> dBm <br> dBm <br> dBm |
| RF to LO Isolation | $\begin{aligned} & \mathrm{f}_{\mathrm{RF}}=250 \mathrm{kHz} \text { to } 800 \mathrm{MHz} \text { (Figure 1) } \\ & \mathrm{f}_{\mathrm{RF}}=700 \mathrm{MHz} \text { to } 1200 \mathrm{MHz} \text { (Figure 2) } \\ & \mathrm{f}_{\mathrm{RF}}=1200 \mathrm{MHz} \text { to } 1700 \mathrm{MHz} \text { (Figure 2) } \\ & \mathrm{f}_{\mathrm{RF}}=1700 \mathrm{MHz} \text { to } 2500 \mathrm{MHz} \text { (Figure 2) } \end{aligned}$ |  | $\begin{aligned} & >61 \\ & >49 \\ & >46 \\ & >43 \end{aligned}$ |  | dB dB dB dB |
| 2RF-2LO Output Spurious Product $\left(f_{R F}=f_{L O}+f_{I F} / 2\right)$ | $\begin{aligned} & \text { 900MHz: } \mathrm{f}_{\mathrm{RF}}=815 \mathrm{MHz} \text { at }-12 \mathrm{dBm}, \mathrm{f}_{\mathrm{IF}}=170 \mathrm{MHz} \\ & 1900 \mathrm{MHz}: \mathrm{f}_{\mathrm{RF}}=1815 \mathrm{MHz} \text { at }-12 \mathrm{dBm}, \mathrm{f}_{\mathrm{IF}}=170 \mathrm{MHz} \end{aligned}$ |  | $\begin{aligned} & \hline-66 \\ & -59 \end{aligned}$ |  | $\begin{aligned} & \mathrm{dBC} \\ & \mathrm{dBC} \end{aligned}$ |
| 3RF-3LO Output Spurious Product $\left(f_{R F}=f_{L O}+f_{I F} / 3\right)$ | $\begin{aligned} & \text { 900MHz: } \mathrm{f}_{\mathrm{RF}}=786.67 \mathrm{MHz} \text { at }-12 \mathrm{dBm}, \mathrm{f}_{\mathrm{IF}}=170 \mathrm{MHz} \\ & 1900 \mathrm{MHz}: \mathrm{f}_{\mathrm{RF}}=1786.67 \mathrm{MHz} \text { at }-12 \mathrm{dBm}, \mathrm{f}_{\mathrm{IF}}=170 \mathrm{MHz} \end{aligned}$ |  | $\begin{aligned} & -83 \\ & -58 \end{aligned}$ |  | $\begin{aligned} & \mathrm{dBC} \\ & \mathrm{dBC} \end{aligned}$ |
| Input 1dB Compression | $\begin{aligned} & \mathrm{RF}=10 \mathrm{MHz} \text { to } 500 \mathrm{MHz} \text { (Figure 1) } \\ & \mathrm{RF}=900 \mathrm{MHz} \text { (Figure 2) } \\ & R \mathrm{RF}=1900 \mathrm{MHz} \text { (Figure 2) } \end{aligned}$ |  | $\begin{aligned} & \hline 10.5 \\ & 10.1 \\ & 6.2 \end{aligned}$ |  | $\begin{aligned} & \mathrm{dBm} \\ & \mathrm{dBm} \\ & \mathrm{dBm} \end{aligned}$ |

Note 1: Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.
Note 2: $45 \mathrm{MHz}, 140 \mathrm{MHz}$ and 450 MHz performance measured on the test circuit shown in Figure 1. $900 \mathrm{MHz}, 1900 \mathrm{MHz}$ and 2450 MHz performance measured on the test circuit shown in Figure 2.

Note 3: Specifications over the $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ temperature range are assured by design, characterization and correlation with statistical process control.
Note 4: SSB Noise Figure measurements performed with a small-signal noise source and bandpass filter on RF input and no other RF signal applied.

## TYPICAL DC PGRFORMANCE CHARACTERISTICS <br> (Test Circuit Shown Figure 2)



## TYPICAL AC PGRFORMANCE CHARACTERISTICS

HF/VHF/UHF Downmixer Application
$\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{EN}=$ High, $\mathrm{P}_{\mathrm{RF}}=-10 \mathrm{dBm}$ (-10dBm/tone for 2-tone IIP3 tests, $\Delta \mathrm{f}=200 \mathrm{kHz}$ ), High-Side LO, $\mathrm{P}_{\mathrm{L} 0}=-5 \mathrm{dBm}$, unless otherwise noted. Test Circuit Shown in Figure 1.


5512 G03

Conv Gain, IIP3 and LO Leakage vs RF Frequency (450MHz App)


Conv Gain, IIP3 and NF
vs LO Power (140MHz App)


5512 G04
Conv Gain, IIP3 and NF vs LO Power (450MHz App)


Conv Gain and IIP3
vs Supply Voltage (140MHz App)


5512 G05
Conv Gain and IIP3
vs Supply Voltage (450MHz App)


## TYPICAL PERFORMANCG CHARACTERISTICS (H9omulz Dowmixier Appiciation)

$V_{C C}=5 \mathrm{~V}, \mathrm{EN}=$ High, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, 1900 \mathrm{MHz}$ RF input matching, $\mathrm{P}_{\mathrm{RF}}=-10 \mathrm{dBm}(-10 \mathrm{dBm} /$ tone for 2-tone IIP3 tests, $\Delta f=200 \mathrm{kHz})$, Low-Side LO, $\mathrm{P}_{\mathrm{LO}}=-10 \mathrm{dBm}$, IF output measured at 170 MHz , unless otherwise noted. Test circuit shown in Figure 2.


5512 G09
Conv Gain, IIP3 and NF
vs LO Input Power


IF Output Power, 2RF-2LO and 3RF-3LO vs RF Input Power


Conv Gain and IIP3
vs Supply Voltage


5512 G10

Output IF Power and Output IM3
vs RF Input Power (2 Input Tones)


5512 G13
2RF-2LO (Half-IF) Spur Level vs LO Input Power


Conv Gain and IIP3 vs Temperature RF $=1900 \mathrm{MHz}, \mathrm{IF}=170 \mathrm{MHz}$


5512 G11

## LO-IF and LO-RF Leakage vs LO Input Power



vs LO Input Power

## PIn fUnCTIOnS

NC (Pins 1, 4, 8, 13, 16): Not connected internally. These pins should be grounded on the circuit board for improved LO to RF and LO to IF isolation.
RF $^{+}$, RF $^{-}$(Pins 2, 3): Differential Inputs for the RF Signal. These pins must be driven with a differential signal. Each pin must be connected to a DC ground capable of sinking 15 mA ( 30 mA total). This DC bias return can be accomplished through the center-tap of a balun, or with shunt inductors. An impedance transformation is required to match the RF input to $50 \Omega$ (or $75 \Omega$ ).
EN (Pin 5): Enable Pin. When the input voltage is higher than 3 V , the mixer circuits supplied through Pins 6, 7, 10, and 11 are enabled. When the input voltage is less than 0.3 V , all circuits are disabled. Typical enable pin input current is $50 \mu \mathrm{~A}$ for $\mathrm{EN}=5 \mathrm{~V}$ and $0 \mu \mathrm{~A}$ when $\mathrm{EN}=0 \mathrm{~V}$.
$\mathbf{V}_{\text {CC1 }}$ (Pin 6): Power Supply Pin for the LO Buffer Circuits. Typical current consumption is 22 mA . This pin should be externally connected to the other $\mathrm{V}_{\mathrm{CC}}$ pins, and decoupled with $0.01 \mu \mathrm{~F}$ and $1 \mu \mathrm{~F}$ capacitors.
$V_{\text {CC2 }}$ (Pin 7): Power Supply Pin for the Bias Circuits. Typical current consumption is 4 mA . This pin should be
externally connected to the other $V_{C C}$ pins, and decoupled with $0.01 \mu \mathrm{~F}$ and $1 \mu \mathrm{~F}$ capacitors.

GND (Pins 9 and 12): Ground. These pins are internally connected to the backside ground for better isolation. They should be connected to RF ground on the circuit board, although they are not intended to replace the primary grounding through the backside contact of the package.
IF-, IF+ (Pins 10, 11): Differential Outputs for the IF Signal. An impedance transformation may be required to match the outputs. These pins must be connected to $\mathrm{V}_{C C}$ through impedance matching inductors, RF chokes or a transformer center-tap.
$\mathrm{LO}^{-}, \mathrm{LO}^{+}$(Pins 14, 15): Differential Inputs for the Local Oscillator Signal. They can also be driven single-ended by connecting one to an RF ground through a DC blocking capacitor. These pins are internally biased to 2V; thus, DC blocking capacitors are required. An impedance transformation or matching resistor is required to match the LO input to $50 \Omega$ (or $75 \Omega$ ).
GROUND (Pin 17): (Backside Contact): Circuit Ground Return for the Entire IC. This must be soldered to the printed circuit board ground plane.

## BLOCK DIAGRAM



## TEST CIRCUITS



| REF DES | VALUE | SIZE | PART NUMBER | REF DES | VALUE | SIZE | PART NUMBER |
| :--- | :---: | :---: | :--- | :--- | :---: | :---: | :--- |
| R1 | $100 \Omega$ | 0402 | AAC CR05-101J | C4 | See Table | 0402 | AVX 0402 |
| C1, C6, C7 | $0.01 \mu \mathrm{~F}$ | 0402 | AVX 04023C103JAT | L1, L2 | See Table | 0402 | Toko LL1005-FH |
| C2 | $1 \mu \mathrm{~F}$ | 0603 | AVX 0603ZD105KAT | T1 | $1: 1$ |  | Coilcraft WBC1-1TL |
| C 3 | 1.8 pF | 0402 | AVX 04025A1R8BAT | T2 | $8: 1$ |  | Mini-Circuits TC8-1 |

Figure 1. Test Schematic for HF/VHF/UHF Downmixer Applications


| REF DES | VALUE | SIZE | PART NUMBER | REF DES | VALUE | SIZE | PART NUMBER |
| :--- | :---: | :---: | :--- | :--- | :---: | :---: | :--- |
| C5, C6, C7 | 100 pF | 0402 | Murata GRP1555C1H101J | L1, L2 | 47 nH | 0402 | Coilcraft 0402CS-47NX |
| C1 | $0.01 \mu \mathrm{~F}$ | 0402 | Murata GRP155R71C103K | L3 | See Table | 0402 | Toko LL1005-FH |
| C2 | $1.0 \mu \mathrm{~F}$ | 0603 | Taiyo Yuden LMK107F105ZA | R1 | 10 | 0402 |  |
| C4 | See Table | 0402 | Murata GRP1555C | T1 | See Table |  | Murata LDB21 Series |
| C3 | See Table | 0402 | Murata GRP1555C | T2 | $8: 1$ |  | Mini-Circuits TC8-1 |

Figure 2. Test Schematic for 900 MHz to 2.5 GHz Downmixer Applications

## APPLICATIONS INFORMATION

The LT5512 consists of a double-balanced mixer, RF buffer amplifier, high-speed limiting LO buffer and bias/enable circuits. The differential RF, LO and IF ports require simple external matching which allows the mixer to be used at very low frequencies, below 1 MHz , or up to 3 GHz . Low side or high side LO injection can be used.
Two evaluation circuits are available. The HF/VHF/UHF evaluation circuit is shown in Figure 1 and the 900 MHz to 2.5 GHz evaluation circuit is shown in Figure 2. The corresponding demo board layouts are shown in Figures 10 and 11, respectively.

## RF Input Port

A simplified schematic of the differential RF input is shown in Figure 3, with the associated external impedance matching elements for a 450 MHz application. Each RF input requires a low resistance DC return to ground


Figure 3. RF Input with External Matching for a 450MHz Application


Figure 4. 450MHz RF Input Matching
capable of sinking 15 mA . This can be accomplished with the center-tap of a balun as shown in Figure 3, or with bias chokes connected from Pins 2 and 3 to ground, if a differential RF input signal is available. The value of the bias chokes should be high enough to avoid reducing the input impedance at the frequency of interest.
Table 1 lists the differential input impedance and differential reflection coefficient between Pins 2 and 3 for several common RF frequencies. As shown in Figures 3 and 4, low-pass impedance matching is used to transform the differential input impedance up to the desired value for the balun input. The following example shows how to design the low-pass impedance transformation network for the RF input.
From Table 1, the differential input impedance at 450 MHz is $18.1+j 5.2$. As shown in Figure 4 , the $5.2 \Omega$ reactance is split, with one half on each side of the $18.1 \Omega$ load resistor. The matching network will consist of additional inductance in series with the internal inductance and a capacitor in parallel with the desired $50 \Omega$ source impedance. The capacitance (C4) and inductance are calculated as follows.

$$
\begin{aligned}
& Q=\sqrt{\left(R_{S} / R_{L}\right)-1}=\sqrt{(50 / 18.1)-1}=1.328 \\
& C 4=\frac{Q}{\omega R_{S}}=\frac{1.328}{2 \pi \cdot 450 \mathrm{MHz} \cdot 50}=9.4 \mathrm{pF} \text { (use 10pF) }
\end{aligned}
$$

$\mathrm{L} 1, \mathrm{~L} 2=\frac{\mathrm{R}_{\mathrm{L}} \cdot \mathrm{Q}}{2 \omega}=\frac{18.1 \cdot 1.328}{2 \cdot 2 \pi \cdot 450 \mathrm{MHz}}$

$$
=4.2 \mathrm{nH} \text { (use } 4.7 \mathrm{nH})
$$

Table 1. RF Input Differential Impedance

| Frequency <br> (MHz) | Differential Input <br> Impedance | Differential S11 |  |
| :---: | :---: | :---: | :---: |
|  |  | Mag | Angle |
| 10 | $18.2+\mathrm{j} 0.14$ | 0.467 | 179.6 |
| 44 | $18+\mathrm{j} 0.26$ | 0.470 | 178.6 |
| 240 | $18.1+\mathrm{j} 2.8$ | 0.471 | 172.6 |
| 450 | $18.1+\mathrm{j} 5.2$ | 0.473 | 166.3 |
| 950 | $18.7+\mathrm{j} 11.3$ | 0.479 | 150.8 |
| 1900 | $20.6+\mathrm{j} 22.8$ | 0.503 | 124.3 |
| 2150 | $21.4+\mathrm{j} 26.5$ | 0.512 | 116.9 |
| 2450 | $22.5+\mathrm{j} 30.5$ | 0.522 | 109.2 |
| 2700 | $24.1+\mathrm{j} 34.7$ | 0.530 | 101.7 |
|  |  |  |  |

LT5512

## APPLICATIONS INFORMATION



Figure 5. RF Input Return Loss
(140MHz, $450 \mathrm{MHz}, 900 \mathrm{MHz}$ and 1900 MHz Matching)
At high frequencies (greater than 900 MHz ), this same matching technique is used, but it is important to consider the IC's input reactance when calculating the external inductance. As shown in Figure 2, the high-frequency evaluation board uses short ( 2 mm ) $72 \Omega$ microstrip lines to realize the required inductance, instead of chip inductors.

External matching values for several frequencies, ranging from 45 MHz to 2.45 GHz are shown in Figures 1 and 2. Measured RF input return losses are plotted in Figure 5.

## LO Input Port

The LO buffer amplifier consists of high-speed limiting differential amplifiers, designed to drive the mixer quad for high linearity. The $\mathrm{LO}^{+}$and $\mathrm{LO}^{-}$pins are designed for differential or single-ended drive. Both LO pins are internally biased to $2 \mathrm{~V}_{\mathrm{DC}}$.


Figure 6. LO Input with Resistive Matching

Table 2. LO Input Differential Impedance

| Frequency <br> (MHz) | Differential Input <br> Impedance | Differential S11 |  |
| :---: | :---: | :---: | :---: |
|  |  | Mag | Angle |
| 750 | $263+j 172$ | 0.766 | -10.2 |
| 1000 | $213+j 178$ | 0.760 | -13.4 |
| 1250 | $175+j 173$ | 0.752 | -16.6 |
| 1500 | $146+j 164$ | 0.743 | -19.8 |
| 1750 | $125+j 153$ | 0.733 | -22.8 |
| 2000 | $108+j 142$ | 0.722 | -25.8 |
| 2250 | $95+j 131$ | 0.709 | -28.9 |
| 2500 | $86+j 122$ | 0.695 | -31.8 |
| 2750 | $78+j 133$ | 0.68 | -34.6 |

A simplified schematic of the LO input is shown in Figure 6 with simple resistive matching and DC blocking capacitors. This is the preferred matching for LO frequencies below 1.5 GHz . The internal (DC) resistance is $400 \Omega$. The required LO drive at the IC is 150 mV RMS (typical) which can come from a $50 \Omega$ source, or a higher impedance source such as PECL. The external matching resistor is required only to reduce the amplitude of the LO signal at the IC, although the input stage will tolerate 10 dB of overdrive without significant performance degradation. Resistive LO port matching is used on the low-frequency evaluation board (see Figure 1).
Above 1.5GHz, the internal capacitance becomes significant and reactive matching to $50 \Omega$ with a single series inductor and DC blocking capacitors is preferred. A schematic is shown in Figure 7. Table 2 lists the differential input


Figure 7. LO Input with Reactive Matching

## APPLICATIONS INFORMATION



Figure 8. Single-Ended LO Port Return Loss vs Frequency for Various Values of L3
impedance and differential reflection coefficient between the $\mathrm{LO}^{+}$and $\mathrm{LO}^{-}$pins. This information can be used to compute the value of the series matching inductor, L3. Alternatively, Figure 8 shows measured LO input return Ioss versus frequency for various values of L3. Reactive LO port matching is used on the high-frequency evaluation board (see Figure 2).

## IF Output Port

The differential IF outputs, $\mathrm{IF}^{+}$and $\mathrm{IF}^{-}$, are internally connected to the collectors of the mixer switching transistors as shown in Figure 9. These outputs should be combined externally through an RF balun or $180^{\circ}$ hybrid to achieve optimum performance. Both pins must be biased at the supply voltage, which can be applied through matching inductors (see Figure 2), or through the center-tap of an outputtransformer(see Figure 1). These pins are protected with ESD diodes; the diodes allow peak AC signal swing up to 1.3 V above $\mathrm{V}_{\text {Cc }}$.
As shown in Table 3, the IF output differential impedance is approximately $390 \Omega$ in parallel with 0.44 pF . A simple band-pass IF matching network suitable for wireless applications is shown in Figure 9. Here, L1, L2 and C3 set the desired IF output frequency. The $390 \Omega$ differential output can then be applied directly to a differential filter, or an 8:1 balun for impedance transformation down to $50 \Omega$. To achieve maximum linearity, C3 should be located as
close as possible to the $\mathrm{IF}^{+} / \mathrm{IF}^{-}$pins. Even small amounts of inductance in series with C3 (such as through a via) can significantly degrade IIP3. The value of C3 should be reduced by the value of internal capacitance (see Table 3). This matching network is simple and offers good selectivity for narrow band IF applications.
For IFfrequencies below 100MHz, the simplest IF matching technique is an 8:1 transformer connected across the IF pins as shown in Figure 1. DC bias to the IF+ and IF- pins is provided through the transformer's center-tap. A small value IF capacitor (C3) improves the LO-IF leakage and attenuates the undesired image frequency. No inductors are required.

Table 3. IF Output Differential Impedance (Parallel Equivalent)

| Frequency (MHz) | Differential Output Impedance | Differential S11 |  |
| :---: | :---: | :---: | :---: |
|  |  | Mag | Angle |
| 10 | 396 II - j10k | 0.766 | 0 |
| 70 | 394 II - j5445 | 0.775 | -1.1 |
| 170 | 393 II - j2112 | 0.774 | -2.8 |
| 240 | 392 II - j1507 | 0.773 | -3.9 |
| 450 | 387 II - j798 | 0.772 | -7.3 |
| 750 | 377 II - j478 | 0.768 | -12.2 |
| 860 | 371 II - j416 | 0.766 | -14.0 |
| 1000 | 363 II - j359 | 0.762 | -16.2 |
| 1250 | 363 II - j295 | 0.764 | -19.6 |
| 1500 | 346 II -j244 | 0.756 | -23.6 |
| 1900 | 317 II - j192 | 0.743 | -29.9 |



Figure 9. IF Output Equivalent Circuit with Band-Pass Matching Elements

PACKAGE DESCRIPTION

## UF Package

16-Lead Plastic QFN ( $4 \mathrm{~mm} \times 4 \mathrm{~mm}$ )
(Reference LTC DWG \# 05-08-1692)


RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS


BOTTOM VIEW-EXPOSED PAD

NOTE:

1. DRAWING CONFORMS TO JEDEC PACKAGE OUTLINE MO-220 VARIATION (WGGC)
2. ALL DIMENSIONS ARE IN MILLIMETERS
3. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE

MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15 mm ON ANY SIDE
4. EXPOSED PAD SHALL BE SOLDER PLATED

## APPLICATIONS InFORMATION



Figure 10. HF/VHF/UHF Evaluation Board Layout (DC933A)


Figure 11. High-Frequency Evaluation Board Layout (DC478B)

## RELATGD PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
| :---: | :---: | :---: |
| Infrastructure |  |  |
| LT5511 | High Linearity Upconverting Mixer | RF Output to 3GHz, 17dBm IIP3, Integrated LO Buffer |
| LT5514 | Ultralow Distortion, IF Amplifier/ADC Driver with Digitally Controlled Gain | 850MHz Bandwidth, 47 dBm OIP3 at 100MHz, 10.5 dB to 33 dB Gain Control Range |
| LT5515 | 1.5 GHz to 2.5 GHz Direct Conversion Quadrature Demodulator | 20dBm IIP3, Integrated LO Quadrature Generator |
| LT5516 | 0.8 GHz to 1.5 GHz Direct Conversion Quadrature Demodulator | 21.5dBm IIP3, Integrated LO Quadrature Generator |
| LT5517 | 40MHz to 900MHz Quadrature Demodulator | 21dBm IIP3, Integrated LO Quadrature Generator |
| LT5519 | 0.7 GHz to 1.4 GHz High Linearity Upconverting Mixer | 17.1 dBm IIP3 at 1GHz, Integrated RF Output Transformer with 50 Matching, Single-Ended LO and RF Ports Operation |
| LT5520 | 1.3GHz to 2.3GHz High Linearity Upconverting Mixer | 15.9 dBm IIP3 at 1.9 GHz , Integrated RF Output Transformer with $50 \Omega$ Matching, Single-Ended LO and RF Ports Operation |
| LT5521 | 10MHz to 3700MHz High Linearity Upconverting Mixer | 24.2 dBm IIP3 at 1.95 GHz , NF $=12.5 \mathrm{~dB}, 3.15 \mathrm{~V}$ to 5.25 V Supply, Single-Ended LO Port Operation |
| LT5522 | 400MHz to 2.7GHz High Signal Level Downconverting Mixer | 4.5V to 5.25V Supply, 25dBm IIP3 at 900MHz, NF $=12.5 \mathrm{~dB}, 50 \Omega$ Single-Ended RF and LO Ports |
| LT5524 | Low Power, Low Distortion ADC Driver with Digitally Programmable Gain | 450MHz Bandwidth, 40dBm OIP3, 4.5dB to 27dB Gain Control |
| LT5525 | High Linearity, Low Power Downconverting Mixer | Single-Ended $50 \Omega$ RF and LO Ports, 17.6 dBm IIP3 at 1900 MHz , $\mathrm{I}_{\mathrm{CC}}=28 \mathrm{~mA}$ |
| LT5526 | High Linearity, Low Power Downconverting Mixer | 3 V to 5.3 V Supply, 16.5 dBm IIP3, 100 kHz to 2 GHz RF , $\mathrm{NF}=11 \mathrm{~dB}$, $\mathrm{I}_{\mathrm{CC}}=28 \mathrm{~mA}$, -65dBm LO-RF Leakage |
| LT5527 | 400MHz to 3.7GHz High Signal Level Downconverting Mixer | Single-Ended $50 \Omega$ RF and LO Ports, 23.5 dBm IIP3 at 1.9 GHz |
| LT5528 | 1.5GHz to 2.4GHz High Linearity Direct I/Q Modulator | 21.8 dBm OIP3 at 2GHz, $-159 \mathrm{dBm} / \mathrm{Hz}$ Noise Floor, $50 \Omega$ Interface at all Ports |

